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## INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

<b>(51) International Patent Classification <sup>7</sup> :</b> <b>C08F 14/18, C08L 27/12, C09J 127/12, B32C 43/00</b>		<b>A2</b>	<b>(11) International Publication Number:</b> <b>WO 00/08071</b>
			<b>(43) International Publication Date:</b> 17 February 2000 (17.02.00)
<b>(21) International Application Number:</b> PCT/US99/17829		<b>(81) Designated States:</b> AE, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, CA, CH, CN, CR, CU, CZ, DE, DK, EE, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MD, MG, MK, MN, MW, MX, NO, NZ, PL, PT, RO, RU, SD, SE, SG, SI, SK, SL, TJ, TM, TR, TT, UA, UG, US, UZ, VN, YU, ZA, ZW, ARIPO patent (GH, GM, KE, LS, MW, SD, SL, SZ, UG, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GW, ML, MR, NE, SN, TD, TG).	
<b>(22) International Filing Date:</b> 6 August 1999 (06.08.99)		<b>Published</b> <i>With declaration under Article 17(2)(a); without abstract; title not checked by the International Searching Authority.</i>	
<b>(30) Priority Data:</b> 60/095,583 6 August 1998 (06.08.98) US			
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<b>(54) Title:</b> MELT-PROCESSIBLE POLY(TETRAFLUOROETHYLENE)			

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**MELT-PROCESSIBLE POLY(TETRAFLUOROETHYLENE)****Field of the Invention**

This invention relates to melt-processible poly(tetrafluoroethylene) (PTFE),  
10 compositions thereof, articles formed therefrom, and methods for making the same.  
More particularly, the present inventions relates to a particular range of  
poly(tetrafluoroethylene) polymers which are readily melt-processible while  
maintaining good/suitable mechanical properties. Further, the present invention  
relates to products made of melt-processible, thermoplastic PTFE compositions.

15

**Background of the Invention**

Poly(tetrafluoroethylene) (PTFE) is well-known for, among other properties,  
its chemical resistance, high temperature stability, resistance against ultra-violet  
radiation, low friction coefficient and low dielectric constant. As a result, it has found  
20 numerous applications in harsh physico-chemical environments and other demanding  
conditions. Equally well-known is the intractability of this important polymer.  
Numerous textbooks, research articles, product brochures and patents state that PTFE  
is intractable because, above its crystalline melting temperature, it does not form a  
fluid phase that is of a viscosity that permits standard melt-processing techniques  
25 commonly used for most thermoplastic polymers (Modern Fluoropolymers, J. Scheirs,  
Ed. Wiley (New York), 1997; The Encyclopaedia of Advanced Materials, Vol. 2, D.  
Bloor et al. Eds., Pergamon (Oxford) 1994; WO 94/02547; WO 97/43102). Suitability  
of a polymer for standard melt-processing techniques may be evaluated, for example,  
through measurement of the melt-flow index of the material (cf. ASTM D1238-88).  
30 Melt-processible polymers should, according to this widely employed method, exhibit  
at least a non-zero value of the melt-flow index, which is not the case for common  
PTFE under testing conditions that are representative of, and comparable to those  
encountered in standard polymer melt-processing. The extremely high viscosity of

PTFE, reported to be in the range of  $10^{10}$ - $10^{13}$  Pa.s at 380 °C, is believed to be associated, among other things, with an ultra-high molecular weight of the polymer, which has been estimated to be in the regime well above 1,000,000 g/mol and often is quoted to be of the order of 10,000,000 g/mol. In fact, it is claimed (Modern  
5 Fluoropolymers, J. Scheirs, Ed. Wiley (New York), 1997, p. 240) that "to achieve mechanical strength and toughness, the molecular weight of PTFE is required to be in the range  $10^7$ - $10^8$  g/mol ...". Due to this high viscosity, common PTFE is processed into useful shapes and objects with techniques that are dissimilar to standard melt-  
10 processing methods. Rods, sheets, membranes, fibers and coatings of PTFE are produced by, for example, ram-extrusion, pre-forming and sintering of compressed powder, optionally followed by machining or skiving, paste-extrusion, high isostatic pressure processing, suspension spinning, and the like, and direct plasma  
polymerization. Unfortunately, these methods generally are less economical than common melt-processing, and, in addition, severely limit the types and characteristics  
15 of objects and products that can be manufactured with this unique polymer. For example, common thermoplastic polymers, such as polyethylene, isotactic polypropylene, nylons, poly(methylmethacrylate) polyesters, and the like, can readily be melt-processed into a variety forms and products that are of complex shapes, and/or exhibit, for example, some of the following characteristics: dense, void-free,  
20 thin, clear or translucent; i.e. properties that are not readily, if at all, associated with products fabricated from PTFE.

The above drawback of PTFE has been recognised virtually since its invention, and ever since, methods have been developed to circumvent the intractability of the polymer. For example, a variety of co-monomers have been introduced in the PTFE  
25 macromolecular chains that lead to co-polymers of reduced viscosity and melting temperature. Co-polymers are those that are polymerized with, for example, hexafluoropropylene, perfluoro(methyl vinyl ether), perfluoro(ethyl vinyl ether), perfluoro(propyl vinyl ether), or perfluoro-(2,2-dimethyl-1,3-dioxole), partially-fluorinated monomers and combinations thereof, in addition to the tetrafluoroethylene  
30 monomer. Several of the resulting co-polymers (for example, those referred to as FEP, MFA, PFA and Teflon<sup>®</sup> AF) provide improved processibility, and can be processed with techniques for common thermoplastic polymers (WO 98/58105). However, a

penalty is paid in terms of some or all of the outstanding properties of the homopolymer PTFE, such as reduced melting temperature and thermal and chemical stability.

Additional methods to process the PTFE homopolymer include, for example, the addition of lubricants, plasticizers, and processing aids, as well as oligomeric polyfluorinated substances and hydrocarbyl terminated TFE-oligomers (for example, Vyda<sup>®</sup> 1000) (US Patents 4,360,488; 4,385,026 and WO 94/02547). The latter method, however, is directed to the improvement of the creep resistance of common PTFE which results in a bimodal morphology with two distinct melting temperatures, and generally does not lead to homogeneous PTFE compositions that can be melt-processed according to standard methods. For example, only a hot-compression molding method is heretofore known for mixtures of standard PTFE and Vyda<sup>®</sup> 1000, that preferably is carried out in the narrow temperature range between about 330 °C to 338 °C. The other aforementioned additions of lubricants, plasticizers, and processing aids also do not yield truly melt-processible PTFE compositions. Solution processing, at superautogeneous pressure, of PTFE from perfluoroalkanes containing 2-20 carbon atoms has been disclosed in WO 94/15998. The latter process is distinctly different from melt-processing methods. Also disclosed is dispersion, and subsequent melt-processing of standard PTFE into thermoplastic (host-) polymers such as polyetheretherketone and polyphenylene sulfide (WO 97/43102) and polyacetal (DE 41 12 248 A1). The latter method compromises important physico-chemical properties of the resulting composition, when compared to neat PTFE, or requires uneconomical and cumbersome removal of the host material.

There exist PTFE grades of low molecular weight and of low viscosity. These grades, which are often referred to as micropowders, commonly are used as additives in inks, coatings and in thermoplastic and other polymers to impart, for example, nucleation, internal lubrication or other desirable properties that, in part, stem from the unique physico-chemical properties of the neat PTFE. Low molecular weight PTFE grades, in their solid form, unfortunately, exhibit extreme brittleness and, according to at least one of the suppliers, these PTFE grades ... " are not to be used as molding or extrusion powders" (Du Pont, Zonyl<sup>®</sup> data sheets and [url:http://www.dupont.com/teflon/fluoroadditives/about.html](http://www.dupont.com/teflon/fluoroadditives/about.html) - July 7, 1998).

Thus, a need continues to exist to develop melt-processible, thermoplastic poly(tetrafluoroethylene)s to exploit the outstanding properties of this polymer in a wider spectrum of product forms, as well as to enable more economical processing of this unique material.

5

#### Summary of the Invention

Surprisingly, it has been found that poly(tetrafluoroethylene)s of a particular set of physical characteristics provide a solution to the above, unsatisfactory situation.

10

Accordingly, it is one objective of the present invention to provide melt-processible, thermoplastic PTFE compositions of good mechanical properties comprising PTFE grades that are characterized as having a non-zero melt-flow index in a particular range. As used hereinafter, the indication "good mechanical properties" means the polymer has properties suitable for use in thermoplastic applications,

15

preferably including applications such as melt-processed thermoplastic formed into unoriented, solid fibers or films exhibiting an elongation at break of at least 10 %, determined under standard ambient conditions at a rate of elongation of 100 % per min.

20

Yet another object of the present invention is to provide melt-processible PTFE of good mechanical properties that exhibit a plateau value of the complex viscosity measured at frequencies below about 0.01 rad/s and at a temperature of 380 °C that is in a range beneficial for processing.

25

Another object of the present invention is to provide melt-processible PTFE that in its unoriented solid form has a crystallinity of between about 1 % and about 60 % and good mechanical properties.

30

Still another object of the present invention is to provide a melt-blending method that yields melt-processible, thermoplastic PTFE compositions of good mechanical properties comprising PTFE grades that are characterized in having a non-zero melt-flow index in a particular range.

Additionally, it is an object of the present invention to provide a method to melt-process PTFE compositions that comprise PTFE grades that are characterized in having a non-zero melt-flow index in a particular range, into useful shapes and articles of good mechanical properties.

Still another object of the present invention is to provide useful shapes and articles of good mechanical properties that are manufactured by melt-processing of PTFE compositions that comprise PTFE grades that are characterized in having a non-zero melt-flow index in a particular range.

5 Yet another object of this invention is to provide novel useful shapes and articles that comprise PTFE.

Additional objects, advantages and novel features of the present invention will be set forth in part in the description which follows, and in part will become apparent to those skilled in the art on examination of the following, or may be  
10 learned by practice of the invention. The objects and advantages of the invention may be realized and attained by means of the instrumentalities and combinations particularly pointed out in the appended claims.

The present invention provides a melt-processible fluoropolymer having a peak melting temperature of at least 320°C and good mechanical properties. And  
15 compositions and articles comprising at least in part a continuous polymeric phase comprising a melt-processible fluoropolymer having a peak melting temperature of at least 320°C and good mechanical properties.

The present invention also provides a composition comprising a melt-processible tetrafluoroethylene polymer, or a melt-processible blend of two or more  
20 tetrafluoroethylene polymers wherein said polymer or said blend of two or more polymers has good mechanical properties. And a process for producing a melt-processible composition comprising a melt-processible tetrafluoroethylene polymer, or a melt-processible blend of two or more tetrafluoroethylene polymers wherein said polymer or said blend of two or more polymers has good mechanical properties. Also  
25 a method for producing an article comprising melt-processing a composition comprising a melt-processible tetrafluoroethylene polymer, or a melt-processible blend of two or more tetrafluoroethylene polymers wherein said polymer or said blend of two or more polymers has good mechanical properties.

30 Another aspect of the present inventions includes using the melt-processible polymer or polymer composition as an adhesive. The present invention provides a process for connecting parts comprising adhering a part to at least one further part with the polymer or composition of the present invention.



### Brief Description of the Drawings

Figure 1 is a stress-strain curve of a melt-processed film of PTFE according to the present invention.

- 5        Figure 2 is a prior art commercial, sintered and skived film of standard (ultra-high molecular weight) PTFE.

### Detailed Description of the Invention

The following is a list of defined terms used herein:

- 10        Void free - refers to a polymer or polymer composition, below its crystallization temperature, having a void content lower than sintered tetrafluoroethylene polymers including sintered tetrafluoroethylene polymers modified up to 0.1 wt% with PPVE (which are reported to have a void content of 2.6% or higher in the Modern Fluoropolymers, J. Scheirs, Ed. Wiley (New York 1997) at p. 15 253). Preferably, void free refers to a polymer or polymer composition, below its crystallization temperature, having a void content lower than 2% as determined by measuring gravimetrically the (apparent) density of a specimen and the intrinsic density via its IR spectroscopically determined amorphous content (as discussed in the Modern Fluoropolymers, J. Scheirs, Ed. Wiley (New York 1997) at pp. 240-255, in 20 particular p. 253; the entire disclosure of which is , 1997, p. 240).

Monomeric units - refers to a portion of a polymer that corresponds to the monomer reactant used to form the polymer. For example,  $-\text{CF}_2\text{CF}_2-$  represents a monomeric unit derived from the monomer reactant tetrafluoroethylene.

### 25        *The poly(tetrafluoroethylene)s*

- The PTFE's according to the present invention generally are polymers of tetrafluoroethylene. Within the scope of the present invention it is contemplated, however, that the PTFE may also comprise minor amounts of one or more co-monomers such as hexafluoropropylene, perfluoro(methyl vinyl ether), 30 perfluoro(propyl vinyl ether), perfluoro-(2,2-dimethyl-1,3-dioxole), and the like, provided, however that the latter do not significantly adversely affect the unique properties, such as thermal and chemical stability of the PTFE homopolymer. Preferably, the amount of such co-monomer does not exceed about 3 mole percent

(herein "mol %"), and more preferably less than about 1 mol %, particularly preferred is a co-monomer content of less than 0.5 mol %. In the case that the overall co-monomer content is greater than 0.5 mol %, it is preferred that amount of the a perfluoro(alkyl vinyl ether) co-monomer is less than about 0.5 mol %; and more preferably less than about 0.2 mol %. Suitable polymers include those having a peak melting temperature, as measured under standard conditions, that exceeds about 320 °C, preferably above 325°C and more particularly above 327°C. Preferably the polymer will have no peak melting temperatures below 320°C and more preferably the polymer will have a single peak melting point which is above 320°C. Most preferred are PTFE homopolymers.

In addition, suitable poly(tetrafluoroethylene)s according to the present invention include those having good mechanical properties, such as, for example, a highly beneficial thermoplastic flow behavior. An indication of the thermoplastic flow behavior of the polymer can be readily analyzed with the commonly employed method of the determination of a melt-flow index (MFI). The latter method, for the present PTFE's is conveniently and reproducibly carried out according to ASTM test D1238-88, at 380 °C under a load of 21.6 kg, herein referred to as the melt flow index or alternatively MFI (380/21.6). Under these experimental conditions, and in a maximum extrudate-collection time of 1 hr, conventional ultra-high molecular weight PTFE grades have an MFI of zero.

Preferably, the PTFE grades according to the present invention have a non-zero MFI (380/21.6) of less than about 2.5 g/10 min in a maximum extrudate-collection time of 1 hr. More preferably, the PTFE's are characterized by an MFI (380/21.6) between about 0.0005 and about 2.5 g/10 min, more preferably between about 0.2 g/10 min and about 2.5 g/10 min and most preferably between 0.25 g/10 min and about 2.5 g/10 min. Although the choice of the PTFE grades used will to some extent depend on the particular end product, an MFI range of about 0.25 to about 2 g/10 min is preferred for most applications. In the case that the PTFE grades according to the present invention comprise a relatively high content of comonomer the upper limit of the MFI range of the preferred grades could be higher. For example, if the PTFE contains up to 3 mol % of comonomer, the upper limit of the MFI range could extend up to about 25 g/10 min, and a preferred range would be between 0.1 up to about 15; when the comonomer content is about 1 mol % or less ,

the MFI range may extend up to about 15 g/ 10 min, more preferably the MFI range would be between 0.1 up to about 10; and at a content of 0.3 mol % or less the suitable MFI would next exceed about 5 g/ 10 min and more preferably would have an MFI value in the above-noted range for PTFE polymers.

5       The highly beneficial thermoplastic flow behavior of the poly(tetrafluoroethylene)s according to the present invention is characterized by their linear visco-elastic behavior, which is conveniently expressed as the absolute value of the complex viscosity. Preferably, the PTFE grades according to the present invention have a plateau value of the complex viscosity measured at frequencies below about  
10   0.01 rad/s and at a temperature of 380 °C of between about  $4 \cdot 10^5$  and about  $10^9$  Pa.s; preferably between about  $7 \cdot 10^5$  and about  $10^8$  more preferably at least  $1.5 \times 10^7$  Pa.s; and most preferred between about  $10^6$  and about  $5 \cdot 10^7$  Pa.s.

      The poly(tetrafluoroethylene)s according to the present invention in addition to having good mechanical properties, are characterized in a relatively low crystallinity  
15   which is beneficial for the toughness of products fabricated thereof. This degree of crystallinity is conveniently determined by differential scanning calorimetry (DSC) according to standard methods known to those skilled in the art of polymer analysis. Preferably, once-molten PTFE grades according to the present invention that are recrystallized by cooling under ambient pressure at a cooling rate of 10 °C/min in  
20   unoriented form have a degree of crystallinity of between about 1 % about 60 %, preferably between about 5 % and about 60%, more preferably at least about 45% and not more than 55% based on a value of 102.1 J/g for 100 % crystalline PTFE (Starkweather, H. W., Jr. et al., J. Polym. Sci., Polym. Phys. Ed., Vol. 20, 751 (1982)).

      Preferably, the PTFE grades according to the present invention are  
25   characterized by an MFI (380/21.6) between about 0.25 to about 2 g/10 min and a degree of crystallinity of once-molten and recrystallized unoriented material of between about 5 %, preferably above 45% and less than about 60 %, preferably less than 55%. More preferably, the PTFE polymer is a polymer having a single peak melting point temperature which is above 325°C and is preferably a homogenous  
30   blend of polymers and/or homopolymer.

      The PTFE grades of the present invention can be synthesized according to standard chemical methods for the polymerization of tetrafluoroethylene as described in detail in the literature (for example, W. H. Tuminello et al., Macromolecules, Vol.

21, pp. 2606-2610 (1988)) and as practiced in the art. Additionally, PTFE grades according to the present invention can be prepared by controlled degradation of common, high molecular weight PTFE, for example by controlled thermal decomposition, electron beam, gamma- or other radiation, and the like (Modern Fluoropolymers, J. Scheirs, Ed. Wiley (New York), 1997 the entire disclosure of which is hereby incorporated by reference). Furthermore, and as demonstrated in the present invention, the PTFE grades according to the present invention can be manufactured by blending of, for example, high melt-flow index grades with appropriate amounts of grades of a lower, for instance below 0.5 g/ 10 min, or even zero melt-flow index to yield mixed materials with values of the melt-flow index, viscosity or crystallinity in the desired range. Due to the relatively simple nature of the MFI-testing method, viscosity measurement and crystallinity determination, using, for example, these analytical tools, those skilled in the art of polymer blending can readily adjust the relative portions of the different PTFE grades to obtain the melt-processible, thermoplastic PTFE compositions according to the present invention.

The present invention also contemplates compositions and articles comprising a continuous phase having at least 15 wt.%, preferably at least 45 wt.%, and more preferably at least 95 wt.% of the melt-processible tetrafluoroethylene polymer including polymers that are formed by blending two or more tetrafluoroethylene polymers of the present invention. An exemplary composition could include a composition or an article wherein the continuous phase composed of at least 99 wt. % of a PTFE homopolymer filled with a filler such as talc, glass and/or other inorganic or organic particles. It may be that the filler comprise a between 10 to 90 wt.%, preferably between 10 and 45 wt % and more preferably less than 30 wt.% of the total composition (including continuous phase and filler).

The compositions according to the present invention optionally may include other polymers, additives, agents, colorants, fillers (*e.g.*, reinforcement and/or for cost-reduction), property-enhancement purposes and the like, reinforcing matter, such as glass-, aramid-, carbon fibers and the like, plasticizers, lubricants, processing aids, blowing or foaming agents, electrically conducting matter, other polymers, including poly(tetrafluoroethylene), fluorinated polymers and copolymers, polyolefin polymers and copolymers, and rubbers and thermoplastic rubber blends, and the like. Depending on the particular application, one or more of the above optional additional ingredients

and their respective amounts are selected according to standard practices known to those skilled in the art of standard polymer processing, compounding and applications.

### *Processing*

5       The PTFE compositions according to the present invention can be processed into useful materials, neat or compounded, single- and multi-component shapes and articles using common melt-processing methods used for thermoplastic polymers that are well known in the art. Typical examples of such methods are granulation, pelletizing, (melt-) compounding, melt-blending, injection molding, melt-blowing, 10 melt-compression molding, melt-extrusion, melt-casting, melt-spinning, blow molding, melt-coating, melt-adhesion, welding, melt-rotation molding, dip-blow-molding, melt-impregnation, extrusion blow-molding, melt-roll coating, embossing, vacuum forming, melt-coextrusion, foaming, calendaring, rolling, and the like.

Melt-processing of the PTFE compositions according to the present invention, 15 in its most general form, comprises heating the composition to above the crystalline melting temperature of the PTFE's, which, of once-molten material, typically are in the range from about 320 °C to about 335 °C (preferably less than 400°C), although somewhat lower, and higher temperatures may occur, to yield a viscous polymer fluid phase. Unlike standard (ultra-high molecular weight) PTFE above its crystalline 20 melting temperature, the PTFE grades according to the present invention form homogenous melts that can be freed from voids and memory of the initial polymer particle morphology. The latter melt is shaped through common means into the desired form, and, subsequently or simultaneously, cooled to a temperature below the crystalline melting temperature of the PTFE's, yielding an object or article of good 25 and useful mechanical properties. In one preferred embodiment, shaped PTFE melts are rapidly quenched at a cooling rate of more than 10 °C/min, more preferably more than 50 °C/min, to below the crystallization temperature to yield objects, such as fibers and films, of higher toughness.

Certain articles, such as, but not limited to, fibers and films made 30 according to the present invention optionally may, subsequently, be drawn or otherwise deformed in one or more directions, embossed, and the like to further improve the physico-chemical, mechanical, barrier, optical and/or surface properties, or be otherwise post-treated (for instance, quenched, heat treated, pressure treated,

and/or chemically treated). The above methods and numerous modifications thereof and other forming and shaping, and post-processing techniques are well known and commonly practiced. Those skilled in the art of processing of thermoplastic polymers are capable of selecting the appropriate melt-processing and optional post-processing  
5 technology that is most economical and appropriate for the desired end product, or product intermediate.

### *Products and Applications*

The products contemplated according to the present invention are numerous,  
10 and cover vastly different fields of applications. This is especially true as PTFE has been approved for food contact and for biomedical applications. Without limiting the scope and use of the present invention, some illustrative products are indicated hereafter. Generally speaking, the products and materials according to the present invention include most or all applications that currently are covered by standard (ultra-  
15 high molecular weight) PTFE, and many of its modified, melt-processible copolymers. In many cases, the present products, when compared with the latter, will have superior physical-chemical properties due to their predominant homopolymer character. Thus, applications are envisioned, among other industries, in the wire and cable industry, the printed-circuit board industry, the chemical processing industry, the  
20 semiconductor industry, the automotive industry, out-door products and coatings industry, the food industry, the biomedical industry, and more generally in industries and uses where any combination of high release, anti-stick, high-temperature stability, high chemical resistance, flame-resistance, anti-fouling, UV resistance, low friction, and low dielectric constant is required.

25 In particular, the PTFE may be used to form at least parts in articles such as, for example, is a wire (and/or wire coating), an optical fiber (and/or coating), a cable, a printed-circuit board, a semiconductor, an automotive part, an outdoor product, a food, a biomedical intermediate or product, a composite material, a melt-spun mono- or multi-filament fiber, an oriented or un-oriented fiber, a hollow, porous or dense  
30 component; a woven or non-woven fabric, a filter, a membrane, a film, a multi-layer- and/or multicomponent film, a barrier film, a container, a bag, a bottle, a rod, a liner, a vessel, a pipe, a pump, a valve, an O-ring, an expansion joint, a gasket, a heat exchanger, an injection-molded article, a see-through article, a sealable packaging, a

profile, and/or a thermoplastically welded part. Preferred articles may include fibers, films, coatings and articles comprising the same.

Typical examples of intermediate and end-user products that can be made according to the present invention include, but are not limited to granulate, thermoplastic composites, melt-spun mono- and multi-filament fibers, oriented and not, hollow, porous and dense, single- and multi-component; fabrics, non-wovens, cloths, felts, filters, gas house filtration bags; sheets, membranes, films (thin and thick, dense and porous); containers, bags, bottles, generally simple and complex parts, rods, tubes, profiles, linings and internal components for vessels, tanks, columns, pipes, fittings, pumps and valves; O-rings, seals, gaskets, heat exchangers, hoses, expansion joints, shrinkable tubes; coatings, such as protective coatings, electrostatic coatings, cable and wire coatings, optical fiber coatings, and the like. The above products and articles may be comprised in part or in total PTFE compositions according to the present invention, or optionally include dissimilar materials, such as for example in multi-layer and multi-component films, coatings, injection molded articles, containers, pipes, profiles, and the like.

Due to the fact that the PTFE grades according to the present invention can be readily processed into mechanical coherent, tough, thin, dense and/or translucent objects, novel application areas for PTFE are contemplated that heretofore were not readily or economically, if at all, accessible due to the intractability of standard (ultra-high molecular weight) grades, notably in areas where the absence of remnants of powder morphology and voids have prohibited use of the latter material. Preferably, the polymer of the present invention has sufficient clarity such that if it were formed into a 1mm thick film, and tested at a temperature below its crystallization temperature, it would be sufficiently translucent to enable images viewed through the film to be readily recognized, preferably without distortion.

Exemplary applications of the polymer and polymer composition of the present which take advantage of some of these beneficial properties include see-through, sealable packaging, barrier films and caps, conformal coatings, dense tubing and linings, thin-walled and complex injection-molded parts, and the like.

The PTFE grades according to the present invention, due to their thermoplastic nature, not only are useful for the simple and economic production of finished goods and intermediate products, but also for other functions. An illustrative example of

such function, without limiting the scope of the present invention, is adhesion and welding. The latter is a well-recognized difficulty associated with common PTFE (Modern Fluoropolymers, J. Scheirs, Ed. Wiley (New York), 1997, p. 251). The PTFE grades according to the present invention were found to be outstanding adhesives, for example, for itself as well as for other fluoropolymers, preferably including common high-molecular weight PTFE products such as films, sheets and the like. Simply by inserting a small amount of a PTFE grade according to the present invention in powder, film or other form between two or more surfaces that one desires to adhere together, liquefying the former material, and subsequently solidifying under slight or modest pressure, it was found to yield a very strong adhesive bond that was provided by the inventive PTFE grades.

The following specific examples are presented to illustrate various aspects of the present invention and are not to be construed as limitations thereon.

## 15 Examples

The following examples are given as particular embodiments of the invention and to demonstrate the practice and advantages thereof. It is understood that the examples are given by way of illustration and are not intended to limit the specification or the claims that follow in any manner.

20

### *General Methods and Materials*

Melt-Flow Index. Values of the melt flow index (MFI) as discussed herein are determined in accordance with the ASTM Standard D1238-88 at a temperature of 380 °C and under a load of 21.6 kg during a maximum extrudate-collection time of 1 hr using a Zwick 4106 instrument.

Viscosity. The absolute values of the complex viscosities of different PTFE grades were measured from small amplitude oscillatory shear experiments (Rheometrics Dynamic Spectrometer RDS-II) at 380 °C for several frequencies between 100 rad/s and  $3.10^{-3}$  rad/s using standard plate-plate geometry. The linear range was estimated from strain-sweep experiments at 100 rad/s.

Thermal Analysis. Thermal analysis was conducted with a Netzsch differential scanning calorimeter (DSC, model 200). Samples of about 5 mg were heated at a standard rate of 10 °C/min. Melting temperatures given hereafter refer to the



endotherm peak temperatures of once molten (at 380 °C) and cooled (at 10 °C/min) material. Crystallinities were determined from the enthalpies of fusion of the same specimen taking the value of 102.1 J/g for 100 % crystalline PTFE (Starkweather, H. W., Jr. et al., J. Polym. Sci., Polym. Phys. Ed., Vol. 20, 751 (1982)).

- 5 Mechanical Data. Tensile tests were carried out with an Instron Tensile Tester (model 4411) at room temperature on dumbbell-shaped specimen of 12 mm gauge length and 2 mm width and fibers. The gauge fiber length was 20 mm. The standard rate of elongation was 100 %/min.

Materials. Various grades of PTFE, purchased from Du Pont (Teflon<sup>®</sup>, Zonyl<sup>®</sup>),

- 10 Ausimont (Algoflon<sup>®</sup>) and Dyneon, were used. The following Table I presents an overview of the melting temperatures and the crystallinities of materials that were once molten at 380 °C and recrystallized by cooling at 10 °C/min, and MFI (380/21.6) of the different grades, which include grades both outside the invention, and those according to the present invention.

Table I

PTFE grade		Melting Temperature* (°C)	Crystallinity (%)	MFI (380/21.6) (g/10 min)	
5	I	Zonyl® 1200	325.9	64.8	>>1,000
	II	Zonyl® 1100	325.0	67.2	>1,000
	III	Zonyl® 1600	329.0	68.9	150
	IV	Dyneon® 9207	329.8	65.1	55
10	V	Zonyl® 1000	329.3	59.5	52
	VI	blend V/XX**	331.6	60.5	35
	VII	Dyneon® 9201	330.5	60.9	22
	VIII	blend V/XX**	331.4	59.9	15
	IX	Zonyl® 1300	329.9	60.5	10
15	X	Algoflon® F5A EX	330.7	61.7	9
	XI	Zonyl® 1400	330.8	57.3	2.8
	XII	Algoflon® L206	332.3	60.8	2.6
	XIII	blend IX/XX**	331.2	51.9	1.8
	XIV	blend XI/XIX**	329.3	49.9	1.2
20	XV	blend V/XIX**	329.4	51.4	1.0
	XVI	blend XI/XIX**	329.7	47.6	0.8
	XVII	blend IX/XX**	330.5	50.9	0.8
	XVIII	blend IX/XX**	331.5	47.5	0.6
	XIX	Zonyl® 1500	327.5	44.2	0.2
25	XX	Teflon® 6	328.6	33.7	0

\*Note: all grades exhibited the well-know thermal transitions around room temperature, typical of PTFE, and only one main melting endotherm at the elevated temperatures above indicated.

\*\*for compositions and preparation of blends see Example 7.

Comparative Example A.

PTFE grades I-XII (Table I) were melt-compression molded at 380 °C with a Carver press (model M, 25 T) for 5 min at 1 metric ton (t), 10 min at 10 t, and then cooled to room temperature during 4 min under 4 t into plaques of about 4 x 4 x 0.1 cm. All grades were found to yield brittle products most of which could not be removed from the mold without fracture. This example shows that neat grades of PTFE of MFI values more than about 2.5 cannot be employed to melt-process articles of useful mechanical properties.

Example 1.

Example A was repeated with PTFE grades XIII-XVIII. The materials were melt-compression molded at 380 °C with a Carver press (model M, 25 T) for 5 min at 1 metric ton (t), 10 min at 10 t, and then cooled to room temperature during 4 min under 4 t into plaques of about 4 x 4 x 0.1 cm. These grades were found to yield mechanically coherent, and translucent samples that could readily be removed from the mold and bend without fracture. This example shows that grades of a non-zero MFI value, but less than about 2.5 can be employed to melt-process articles of PTFE of useful mechanical properties.

Comparative Example B.

Attempts were made to melt-compression mold at 380 °C with a Carver press (model M, 25 T) films of PTFE grades I-XII. All grades were found to yield brittle products that could not be mechanically removed from the mold without fracture. This example shows that neat grades of MFI values more than about 2.5 cannot be employed to produce melt-processed, free-standing films of useful mechanical properties.

Example 2.

Example B was repeated with PTFE grades XIII-XVIII. The materials were melt-compression molded at 380 °C with a Carver press (model M, 25 T) for 5 min at 1 metric ton (t), 10 min at 10 t, and then cooled to room temperature during 4 min under 4 t into thin films of about 15 x 15 x about 0.025 cm. These grades were

found to yield mechanically coherent, translucent and flexible films that could readily be removed from the mold. This example shows that grades of a non-zero MFI value, but less than about 2.5 can be employed to melt-process thin, mechanically coherent films of PTFE.

5                   The mechanical properties of the melt-processed PTFE films were measured according to the standard method detailed above. A typical stress-strain curve is presented in Fig. 1 (A), for comparison purposes, together with that of a sample of commercial, pre-formed/sintered and skived film of 0.40 mm thickness (B). This figure shows that the melt-processed PTFE film (here of grade XVI (Table I))  
10 has the typical deformation properties of a thermoplastic, semi-crystalline polymer with a distinct yield point and strain hardening. The stress-strain curves A and B resemble each other, which indicates that these melt-processed PTFE films do not have substantially inferior mechanical properties when compared to common, PTFE of ultra-high molecular weight. The mechanical data of the two products are collected  
15 in Table II.

Table II

PTFE film	Yield Stress (MPa)	Tensile Strength (Nominal, MPa)	Elongation at Break (%)
Skived Film	12.8	36.1	476
Melt-processed Film of PTFE grade XVI	12.6	20.9	427

25                   The excellent mechanical properties of the film according to the present invention were not affected by storing the sample for periods in excess of 15 hrs at temperatures of 200 °C and higher.

30                   In addition, we observed that the melt-processed PTFE films, unlike the commercial skived material, were dense and translucent, through which text readily could be read up to a film thickness of about 1 mm.

### Comparative Example C.

PTFE grades I-XII and XX were introduced into a laboratory melt-spinning apparatus (SpinLine, DACA Instruments), the temperature of which was kept at 380 °C, and that was equipped with a die of 1 mm diameter (length/diameter ratio 1). PTFE grades I-XII could not be collected as monofilaments due to brittleness of the extrudate, leading to premature fracture. Ultra-high molecular weight PTFE grade XX could not be melt-spun, even at loads up to 5 kN (limit of equipment), due to the high viscosity (zero MFI) of the material.

### Example 3.

Example C was repeated with PTFE grade XV. PTFE monofilaments were collected onto bobbins. The filaments were tough, and could readily be drawn at room temperature to draw ratios exceeding 4.

The mechanical properties of the melt-spun fibers were measured according to the method detailed above. Their tensile strength exceeded 0.1 GPa.

### Comparative Example D.

PTFE grades I-XII and XX were introduced into a laboratory, recycling twin-screw extruder (MicroCompounder, DACA Instruments), the temperature of which was kept at 380 °C, and that was equipped with an exit die of 2 mm diameter. PTFE grades I-XII could not be collected as continuous extrudates due to extreme brittleness of the extrudate, leading to premature fracture. Ultra-high molecular weight PTFE grade XX could not be extruded due to the high viscosity (zero MFI) of the material.

### Example 4.

Example D was repeated with PTFE grades XIII-XVIII. Continuous PTFE extrudates were readily collected. The extrudates could readily be chopped into granulate or drawn into monofilaments.

### Example 5.

PTFE grade XV was melt-compounded at 380 °C in a Brabender DSK25 segmented, co-rotating extruder (25 mm diameter; 22 aspect ratio) with 0.1

weight % of various dyes (Amaplast<sup>®</sup> Blue HB, Red RP, Yellow NX, ColorChem Int. Corp.), 10 % of TiO<sub>2</sub> (Fluka), 10 weight % of aramid pulp (Twaron<sup>®</sup>, Akzo Nobel), and 20 weight % of chopped, 15 mm long carbon fiber, respectively. Subsequently, the compounded materials obtained were melt-processed into plaques according to the method in Example 1. Optical microscopy on thin sections (about 0.1 mm) revealed that in all cases extremely homogeneous mixtures and composites were obtained. This example shows that PTFE according to the present invention can be melt-compounded.

10 Comparative Example E.

Two strips of about 7 x 1 x 0.04 cm of commercial, skived film of high molecular weight PTFE were pressed together in a Carver press (model M, 25T) at a temperature of 380 °C under a load of less than 1 t for 2 min and subsequently cooled to room temperature. Without much force, the strips could be separated from each other, which is indicative of poor adhesion, and illustrates the difficulties encountered in welding of common PTFE.

Example 6.

Example E was repeated. However, a small piece of melt-processed film of PTFE grade XV (about 1 x 1 x 0.02 cm) was placed in between the two strips of about 7 x 1 x 0.04 cm of commercial, skived film of high molecular weight PTFE. This sandwich structure was also pressed together in a Carver press (model M, 25T) at a temperature of 380 °C under a load of less than 1 t for 2 min and, subsequently, cooled to room temperature. The strips could be separated from each other only after one or both of the skived material strips exhibited excessive plastic deformation, which is indicative of outstanding adhesive properties of this grade to, for example, common PTFE.

Example 7.

Various amounts (total quantity 90 g) of PTFE grades V and XIX, XI and XIX, and IX and XX, respectively, (see Table 1) were introduced into a Brabender melt-kneader (model Plasti-corder PL 2000), which was kept at a temperature of about

380 °C, 60 rpm. After about 1 min, a clear homogeneous melt was formed that behaved like a melt of ordinary thermoplastics. Mixing was continued for 10 min, after which the blended product was discharged. The MFI values of the different blends were measured. The results are given in Table III.

5

Table III

	PTFE grades	Weight Ratio	MFI (380/21.6)
		(-)	(g/10 min)
10	IX + XX	45 -55	0.6
	IX + XX	50 - 50	0.8
	XI + XIX	10-90	0.8
	V + XIX	12.5-87.5	1.0
	XI + XIX	25-75	1.2
15	IX + XX	60 - 40	1.8

This example shows that PTFE grades according to the present invention of an MFI value in the desired range can be prepared by melt-blending of PTFE grades of which one or more are of too high or/and too low values of their respective MFI.

20

#### Example 8.

Various amounts (total quantity 90 g) of PTFE grades V and XIX, and IX and XX, respectively, (see Table 1) were introduced into a Brabender melt-kneader (model Plasti-corder PL 2000), which was kept at a temperature of about 380 °C, 60 rpm. After about 1 min, a clear homogeneous melt was formed that behaved like a melt of ordinary thermoplastics. Mixing was continued for 10 min, after which the blended product was discharged. The absolute values of the complex viscosities of various PTFE samples were measured from small amplitude oscillatory shear experiments. The results are given in Table IV.

30

Table IV

5	PTFE grades	Weight Ratio	Viscosity
		(-)	(Pa.s)
10	V + XIX	60-40	9.3. 10 <sup>5</sup>
	V + XIX	40-60	5.5. 10 <sup>6</sup>
	V + XIX	20-80	8.4. 10 <sup>6</sup>
	V + XIX	10-90	1.3. 10 <sup>7</sup>
	IX + XX	60-40	1.2. 10 <sup>7</sup>
	IX + XX	50-50	1.8. 10 <sup>7</sup>
	IX + XX	45-55	2.4. 10 <sup>7</sup>

15

The same PTFE samples were processed into films according to the method in Example 2. All films were found to exhibit good mechanical properties.

Having described specific embodiments of the present invention, it will be understood that many modifications thereof will readily appear or may be suggested to those skilled in the art, and it is intended therefore that this invention is limited only by the spirit and scope of the following claims.

20



What is claimed is:

1. A melt-processible fluoropolymer having a peak melting temperature of at least 320°C and good mechanical properties.

5

2. The fluoropolymer according to claim 1 wherein the fluoropolymer has an elongation at break of greater than 10%.

3. The fluoropolymer according to any one of claims 1-2 wherein said  
10 fluoropolymer has a melt-flow index of greater than 0.2 g/10 min and less than 2.5 g/10 min.

4. The fluoropolymer according any one of claims 1-3 wherein said  
15 fluoropolymer is polytetrafluoroethylene.

5. The fluoropolymer according to any one of claims 1-4 wherein the fluoropolymer comprises a minor amount of at least one or more fluoro-monomeric units different from a tetrafluoroethylene monomeric unit.

20 6. The fluoropolymer according to any one of claims 1-5 wherein said fluoropolymer comprises at least one or more fluoro-monomeric units derived from hexafluoropropylene, perfluoro(alkyl vinyl ether), and/or perfluoro-(2,2,-dimethyl-1,3-dioxole).

25 7. The fluoropolymer according to any one of claims 5-6 wherein the amount of said at least one or more fluoro-monomeric units in said fluoropolymer is less than 3 mol %.

8. The fluoropolymer according to any one of claims 5-6 wherein the  
30 amount of fluoro-monomeric units derived from perfluoro(alkyl vinyl ether) in said fluoropolymer is less than 0.5 mol %.

9. The fluoropolymer according to any one of claims 1-8 wherein the fluoropolymer, after being once molten, has a crystallinity of between 1% and 60%.

10. The fluoropolymer according to any one of claims 1-9 wherein the fluoropolymer has an absolute value of the complex viscosity, measured at 0.01 rad/s, of between  $1.5 \times 10^7$  Pa.s and  $10^9$  Pa.s.

11. The fluoropolymer according to any one of claims 1-10 wherein the fluoropolymer is void free.

12. The fluoropolymer according to any one of claims 1-11 wherein a 1mm thick film of said fluoropolymer is sufficiently clear, at a temperature below its crystallization temperature, to enable images viewed through the film to be readily recognized.

13. A composition comprising a continuous polymeric phase comprising the fluoropolymer according to any one of claims 1-12.

14. The composition according to claim 13 wherein the composition comprises a continuous phase having at least about 15 wt % of said fluoropolymer.

15. An article comprising the fluoropolymer according to any one of claims 1-14.

16. The article of claim 15 wherein the article is formed at least in part by melt processing said fluoropolymer.

17. The article according to any one of claims 15-16 wherein said article is a wire, an optical fiber, a cable, a printed-circuit board, a semiconductor, an automotive part, an outdoor product, a food, a biomedical intermediate or product, a composite material, a melt-spun mono- or multi-filament fiber, an oriented or un-oriented fiber, a hollow, porous or dense component; a woven or non-woven fabric, a filter, a membrane, a film, a multi-layer- and/or multicomponent film, a barrier film, a

container, a bag, a bottle, a rod, a liner, a vessel, a pipe, a pump, a valve, an O-ring, an expansion joint, a gasket, a heat exchanger, an injection-molded article, a see-through article, a sealable packaging, a profile, and/or a thermoplastically welded part.

5           18.     The article according to any one of claims 15-17 wherein said fluoropolymer adheres two more parts together wherein at least one of said parts comprises tetrafluoroethylene polymer.

            19.     A composition comprising:  
10           a melt-processible tetrafluoroethylene polymer, or  
            a melt-processible blend of two or more tetrafluoroethylene polymers wherein said polymer or said blend of two or more polymers has good mechanical properties.

            20.     The composition according to claim 19 wherein said polymer or said  
15           blend of two or more polymers has a peak melting temperature of at least 320°C.

            21.     The composition according to any one of claims 19-20 wherein said polymer or said blend of two or more polymers has a melt flow index of greater than 0.2 g/10 min and less than 2.5 g/10 min.  
20

            22.     The composition according to any one of claims 19-21 wherein said polymer or said blend of two or more polymers has an elongation at break of greater than 10%.

25           23.     The composition according to any one of claims 19-22 wherein said polymer or at least one polymer of said blend of two or more polymers comprises a minor amount of at least one or more fluoro-monomeric units different from a tetrafluoroethylene monomeric unit.

30           24.     The composition according to claim 23 wherein said at least one or more fluoro-monomeric units is derived from hexafluoropropylene, perfluoro(alkyl vinyl ether), and perfluoro-(2,2,-dimethyl-1,3-dioxole).

25. The composition according to any one of claims 23-24 wherein the amount of said at least one or more fluoro-monomeric units in said polymer or in said at least one polymer of said blend of two or more polymers is less than 3 mol %.

5        26. The composition according to any one of claims 23-25 wherein the amount of fluoro-monomeric units derived from perfluoro(alkyl vinyl ether) in said polymer or in said at least one polymer of said blend of two or more polymers is less than 0.5 mol %.

10       27. The composition according to any one of claims 19-26 wherein said polymer or said blend of two or more polymers, after being once molten, has a crystallinity of between 1% and 60%.

15       28. The composition according to any one of claims 19-27 wherein said polymer or said blend of two or more polymers has a melt-flow index of between 0.25 g/10 min and 2g/10 min.

20       29. The composition according to any one of claims 19-28 wherein said polymer or said blend of two or more polymers has an absolute value of the complex viscosity, measured at 0.01 rad/s, of between  $1.5 \times 10^7$  Pa.s and  $10^9$  Pa.s.

25       30. The composition according to any one of claims 19-29 wherein the composition further comprises other polymers, fillers, additives, agents, and/or colorants.

30       31. The composition according to any one of claims 19-30 wherein the composition further comprises other fluorinated polymers and/or copolymers, polyolefin polymers and/or copolymers, and/or rubbers and/or thermoplastic rubber blends.

32. The composition according to any one of claims 19-31 wherein the composition is void free.

33. The composition according to any one of claims 19-32 wherein a 1mm thick film of the composition is translucent, at a temperature below its crystallization temperature.

5 34. A method for producing a melt-processible composition comprising:  
forming a polymer composition according to any one of claims 19-33.

35. The method according to claim 34 wherein said polymer or at least one of said blend of two or more polymers is formed at least in part by polymerizing  
10 tetrafluoroethylene.

36. The method according to any one of claims 34-35 wherein said polymer or at least one of said blend of two or more polymers is formed at least in part by degrading a tetrafluoroethylene polymer.  
15

37. The method according to any one of claims 34-36 wherein said polymer or said blend of polymers is formed at least in part by blending two or more tetrafluoroethylene polymers.

20 38. The method according to any one of claims 34-37 wherein the polymer composition is formed at least in part by blending one or more polymers or polymer mixtures having a melt flow index of less than 0.5 g/10 min.

39. The method according to any one of claims 34-38 wherein the melt-  
25 processible composition is formed into an article.

40. A method for producing an article comprising  
melt-processing a composition comprising:  
a melt-processible tetrafluoroethylene polymer, or  
30 a melt-processible blend of two or more tetrafluoroethylene polymers  
wherein said polymer or said blend of two or more polymers has good mechanical properties.

41. The method according to claim 40 wherein said polymer or said blend of two or more polymers has an elongation at break of greater than 10%.

42. The method according to any one of claims 40-41 wherein said  
5 polymer composition has a melt-flow index of greater than 0 g/10 min and less than 25 g/10 min.

43. The method according to any one of claims 40-42 wherein the melt-processible composition has a complex viscosity, measured at 0.01 rad/s, of between 4  
10  $\times 10^5$  Pa.s and  $10^9$  Pa.s.

44. The method according to any one of claims 40-43 wherein the melt-processible composition, after being once molten, has a crystallinity of between 1% and 60%.

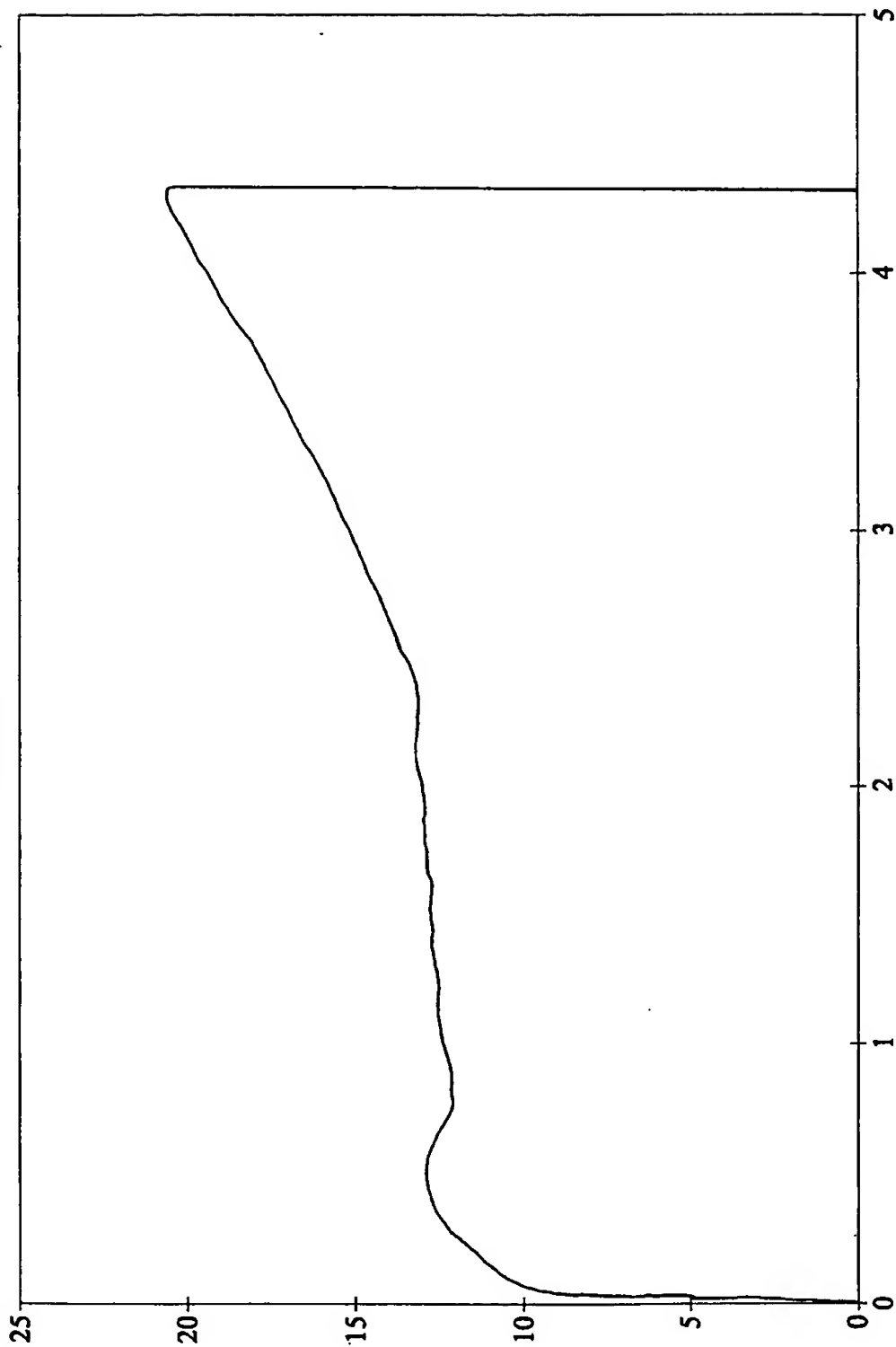
45. The method according to any one of claims 40-44 wherein melt-processing includes granulating, pelletizing, melt-compounding, melt-blending, injection molding, melt-blowing, melt-compression molding, melt-extruding, melt-casting, melt-spinning, blow-molding, melt-coating, melt-adhering, welding, melt-  
20 rotating, molding, dip-blow-molding, melt-impregnating, extrusion blow-molding, melt-roll coating, embossing, vacuum forming, melt-coextruding, foaming, calendering and/or rolling.

46. A process for connecting parts comprising:  
25 adhering a part to at least one further part with the composition according to any one of claims 19-33.

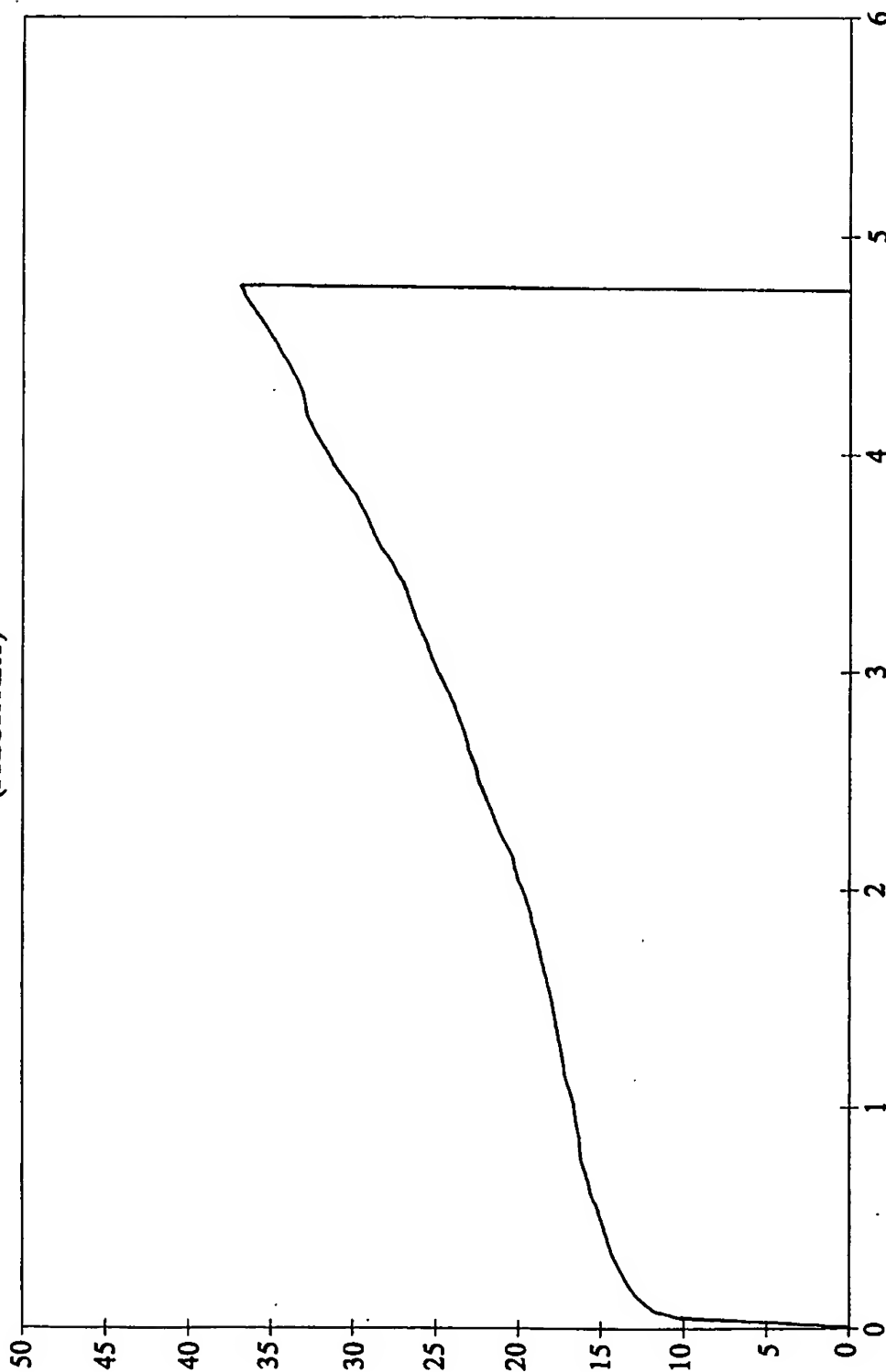
47. The process according to claim 46 wherein at least one of said parts comprises a fluoropolymer.

30 48. The process according to any one of claims 46-47 wherein at least one of said parts comprises tetrafluoroethylene polymer.

*FIG. 1*



**FIG. 2**  
(PRIOR ART)





# PATENT COOPERATION TREATY

# PCT

## DECLARATION OF NON-ESTABLISHMENT OF INTERNATIONAL SEARCH REPORT

(PCT Article 17(2)(a), Rules 13ter.1(c) and Rule 39)

Applicant's or agent's file reference <b>SMITH240098</b>	IMPORTANT DECLARATION	Date of mailing (day/month/year) <b>22/12/1999</b>
International application No. <b>PCT/US 99/ 17829</b>	International filing date (day/month/year) <b>06/08/1999</b>	(Earliest) Priority date (day/month/year) <b>06/08/1998</b>
International Patent Classification (IPC) or both national classification and IPC <b>C08F14/18, C08L27/12, C09J127/12, B32C43/00</b>		
Applicant <b>OMLIDON TECHNOLOGIES LLC et al.</b>		

This International Searching Authority hereby declares, according to Article 17(2)(a), that no International search report will be established on the international application for the reasons indicated below

1. ☐ The subject matter of the international application relates to:
  - a. ☐ scientific theories.
  - b. ☐ mathematical theories
  - c. ☐ plant varieties.
  - d. ☐ animal varieties.
  - e. ☐ essentially biological processes for the production of plants and animals, other than microbiological processes and the products of such processes.
  - f. ☐ schemes, rules or methods of doing business.
  - g. ☐ schemes, rules or methods of performing purely mental acts.
  - h. ☐ schemes, rules or methods of playing games.
  - i. ☐ methods for treatment of the human body by surgery or therapy.
  - j. ☐ methods for treatment of the animal body by surgery or therapy.
  - k. ☐ diagnostic methods practised on the human or animal body.
  - l. ☐ mere presentations of information.
  - m. ☐ computer programs for which this International Searching Authority is not equipped to search prior art.
2. ☒ The failure of the following parts of the international application to comply with prescribed requirements prevents a meaningful search from being carried out:
 

☐ the description
☒ the claims
☐ the drawings
3. ☐ The failure of the nucleotide and/or amino acid sequence listing to comply with the standard provided for in Annex C of the Administrative Instructions prevents a meaningful search from being carried out:
 

☐ the written form has not been furnished or does not comply with the standard.  
☐ the computer readable form has not been furnished or does not comply with the standard.
4. Further comments:

SEE ANNEX

Name and mailing address of the International Searching Authority European Patent Office, P.B. 5818 Patentlaan 2 NL-2280 HV Rijswijk Tel. (+31-70) 340-2040, Tx. 31 651 epo nl, Fax: (+31-70) 340-3016	Authorized officer <b>Nathalie Ostwinkel</b>
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## FURTHER INFORMATION CONTINUED FROM PCT/ISA 203

The Claims relate to melt-processible fluoropolymers (claims 1-12 and 19-33), compositions (claims 13, 14 and 19-33), articles (claims 15-18), methods (claims 34-45) and processes (claims 46-48) which are characterized in terms of the physical properties of the fluoropolymer or its compositions: peak melting temperature (claims 1 and 20), 'good mechanical properties' (claims 1, 19 and 40), elongation at break (claims 2, 22 and 41), melt-flow index (claims 3, 21, 28, 38 and 42), crystallinity (claims 9, 27 and 44), complex viscosity (claims 10, 29 and 43), 'void free' (claims 11 and 32), 'sufficient clear' (claim 12) and 'translucent' (claim 33).

However, the claims and the description do not contain indications which would enable the person skilled in the art to obtain or prepare the fluoropolymers, compositions and articles as claimed or to carry out the methods or processes as claimed, contrary to Art. 5 PCT.

It may be seen in the description (see examples and Table III) that some particular combinations of fluoropolymers appear to have (at least some of) the physical properties which are recited in the claims, but these fluoropolymers are characterized solely by their generic trade names (generic in the sense that ie., 'Zonyl (TM) 1100' is not known, but 'Zonyl (TM) MP 1100' is a commercial PTFE grade manufactured by Dupont, etc.). Additionally, not a single one of the fluoropolymer combinations which are used in the examples on file, or any reasonable generalisation thereof, may be found in the claims.

Further, the description at page 9, lines 6-15 acknowledges that 'the desired result to be achieved is a matter of experimentation which is readily available to the person skilled in the art', adding thus further uncertainty when coming to determine the technical features on which the invention may be based.

Furthermore, the application shows on Table I, description page 15, that several commercial polymer grades as purchased already have the characteristics claimed in (at least) claims 1 and 20.

Thus, claims 1-48 attempt to define the claimed subject-matter in terms of the result to be achieved, which merely amounts to a statement of the underlying problem to be solved. The technical features necessary for achieving this result are thus absent from the claims and the description.

Therefore, according to Art. 5 PCT, the subject-matter of present claims 1-48, even when taking carefully in consideration the technical content and explanations included in the description in its entirety, cannot be the subject of an international search report because the features which are necessary in order to perform the invention are not disclosed in the application and thus it is not possible to determine on which technical features a search report could be based.

The applicant's attention is drawn to the fact that claims relating to inventions in respect of which no international search report has been established need not be the subject of an international preliminary examination (Rule 66.1(e) PCT). The applicant is advised that the EPO policy when acting as an International Preliminary Examining Authority is

FURTHER INFORMATION CONTINUED FROM PCT/ISA/ 203

normally not to carry out a preliminary examination on matter which has not been searched. This is the case irrespective of whether or not the claims are amended following receipt of the search report or during any Chapter II procedure. If the application proceeds into the regional phase before the EPO, the applicant is reminded that a search may be carried out during examination before the EPO (see EPO Guideline C-VI, 8.5), should the problems which led to the Article 17(2) declaration be overcome.